AIRCRAFT SERIOUS INCIDENT INVESTIGATION REPORT

PRIVATELY OWNED
JA4010

June 28, 2018



The objective of the investigation conducted by the Japan Transport Safety Board in accordance with the Act for Establishment of the Japan Transport Safety Board and with Annex 13 to the Convention on International Civil Aviation is to prevent future accidents and incidents. It is not the purpose of the investigation to apportion blame or liability.

Kazuhiro Nakahashi Chairman Japan Transport Safety Board

Note:

This report is a translation of the Japanese original investigation report. The text in Japanese shall prevail in the interpretation of the report.

AIRCRAFT SERIOUS INCIDENT INVESTIGATION REPORT

UNABLE TO MOVE ON RUNWAY DUE TO DAMAGES ON NOSE LANDING GEAR AT FUKUSHIMA AIRPORT, JAPAN AT AROUND 14:00 JST, JUNE 27, 2017

PRIVATELY OWNED PIPER PA-46-310P, JA4010

June 8, 2018

Adopted by the Japan Transport Safety Board

Chairman Kazuhiro Nakahashi

Member Toru Miyashita

Member Toshiyuki Ishikawa

Member Yuichi Marui Member Keiji Tanaka

Member Miwa Nakanishi

1. PROCESS AND PROGRESS OF INVESTIGATION

1.1 Summary of	On Tuesday, June 27, 2017, a privately owned Piper PA-46-310P,		
the Serious Incident	registered JA4010, damaged the nose landing gear during its landing		
	roll on runway 01 at Fukushima Airport, therefore, the aircraft became		
	unable to move on the Runway.		
1.2. Outline of the	This event fell under the category of "Case where the landing gear		
Serious Incident	is damaged and thus flight of the subject aircraft could not be		
Investigation	continued" as stipulated in item 8, Article 166-4 of the Ordinance for		
	Enforcement of Civil Aeronautics Act (Ordinance of Ministry of		
	Transport No. 56 of 1952), and was classified as a serious incident.		
	On June 27, 2017, the Japan Transport Safety Board (JTSB)		
	designated an investigator-in-charge and an investigator to investigate		
	this serious incident.		
	An accredited representative of the United States, as the State of		
	Design and Manufacture of the aircraft involved in this serious incident,		
	participated in the investigation.		

Comments were invited from the parties relevant to the cause of the serious incident and the relevant state.

2. FACTUAL INFORMATION

2.1 History of the Flight

According to the statements of the pilot (hereinafter referred to as "the Pilot") and passenger, the history of the flight is summarized as follows.

At 13:18 Japan Standard Time (JST: UTC + 9hrs, unless otherwise stated, all times are indicated in JST on a 24-hour clock) on June 27, 2017, a privately owned Piper PA-46-310P, registered JA4010, took off Honda



Photo 1: Aircraft involved in the Serious Incident

Airport bound for Fukushima Airport for a familiarization flight with the Pilot in the left seat and a passenger in the right seat.

When the aircraft landed on runway 01 at Fukushima Airport after conducting ILS approach both the Piot and the passenger confirmed that the landing gears were locked in the extended position using three green lights respectively.

The indicated airspeed of the aircraft is 85 kt during approach when conducting normal landing, and the Pilot confirmed that the indicated airspeed was 81-82 kt just before the threshold of runway 01. The speed when the aircraft touched down was unknown, but the aircraft landed without large impact at around the end of the aiming point marking.

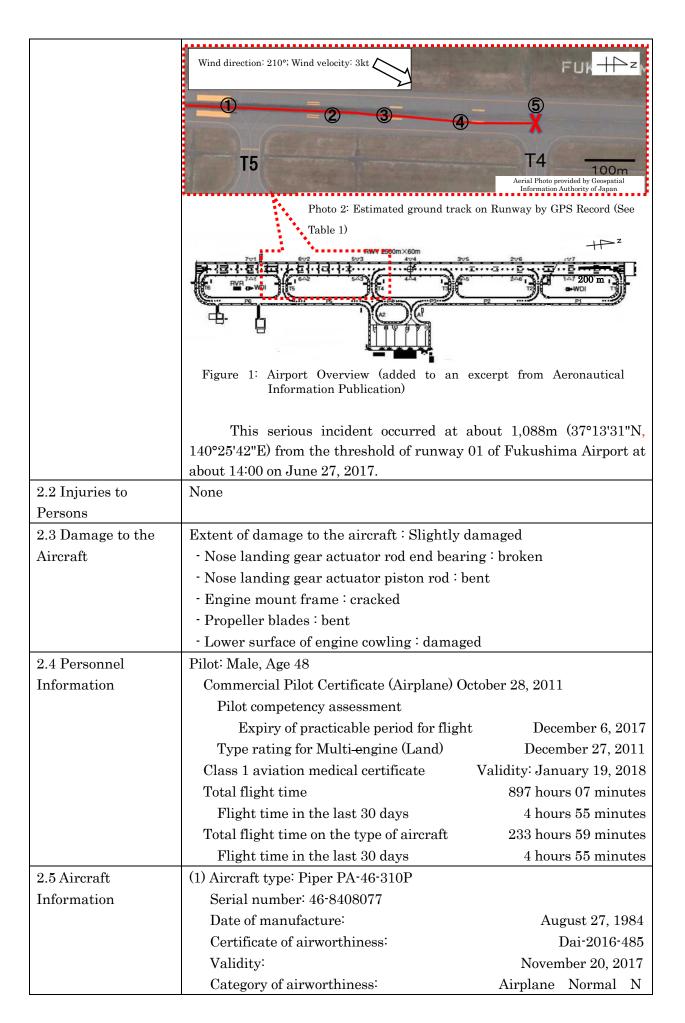
Since there was a long distance from the touchdown point to the taxi-way T4 where the Pilot planned to vacate the runway, the Pilot did not apply the brakes and was using only the rudder pedals to keep rolling on the runway centerline.

The aircraft, after running straight on the runway for a while, gradually started drifting from the runway center line towards the right and at the same time its nose was going to go down. Since all three green lights to indicate fully extended position of the landing gears had stayed illuminating, the passenger judged the nose tire went flat then he said "Nose tire, Flat tire". The Pilot pulled up the control column to make the nose up, however, the nose kept going down. Finally, the Pilot heard the noise of propeller blades hitting the runway.

Afterward, the aircraft moved on the runway under the condition its lower part of the forward fuselage was contacting the runway, it stopped intersection between the runway and taxiway T4.

After reporting to an Air Traffic Service Flight Information Officer at Fukushima Airport Mobile Communication Station that the nose landing gear of the aircraft had been damaged and the aircraft had to stop on the runway, the Pilot and passenger evacuated from the aircraft.

Besides, the Pilot found no anomaly while performing the exterior inspection before the flight.



	m . 1		0.04/1	
	Total flight time:		3,044 hours 04 minutes	
		light time since the last periodical check (100-hour inspection on		
	March 18, 2017)		45 hours20 minutes	
			the time of occurrence of this	
	serious incident, b	ooth of the weight	and position of the center of	
	gravity of the aircr	aft were within the	e allowable range.	
2.6 Meteorological	Weather information provided by an Air Traffic Service Flight			
Information	Information Officer at Fukushima Airport at 13:55			
	Wind direction 2	10°; Wind velocity	3kt; Temperature 22°C,	
	QNH 29.90 inHg			
2.7 Additional	(1) Information on the airport			
Information	Fukushima Airport has a runway with a length of 2,500 m, a			
	width of 60 m, and the runway direction of 01/19. Its surface is paved			
	with asphalt-concrete			
	(2) Approach and land			
	The Flight Manual of the aircraft includes the following			
	descriptions in "Section 4: Normal Procedures." (Excerpt)			
	16. Approach and la			
	a. Normal Procedures (not shown in the Performance Table)			
	When a runway length is sufficiently longer than the			
	required length, the normal approach and landing method can			
	be used. Set the engine power that is required to maintain the			
	desired approach path angle and descend on the final approach			
	course at 85 KIAS. The flap angle during the approach and			
	landing as well as speed at the time of the touch down on the			
	runway should be selected depending on the condition of the			
	runway surface, wind, and aircraft weight. It is generally			
	desirable to touch down at the speed as low as possible that is			
	acceptable to the landing conditions. The landing distance when			
	this method is applied is not described in the Performance Table			
	because it varies from one landing to another landing.			
	Based on the sc	ratches of the pro	peller blades of the aircraft on	
	the runway surface, the speed of the aircraft when its blades hit the			
	surface is estimated to be about 45 kt.			
	(3) Distance from run	way approach end		
	The distance from the runway threshold corresponding from ① to			
	⑤ on Photos 2 is as f	ollows:		
	No. Situation	of Aircraft and	Distance from Runway	
	Scratche	es on runway	Threshold (m)	
	① Touchdown po	oint	460	
	② Tire marks de	eflected to the	740–	
	right			
		propeller blades	756–	
	4 Paint marks l		811-	
	landing gear			
	landing gear	door		

Stop position 1,088

Table 1: Distance from Runway Threshold

(4) Information on damage

Both of two propeller blades of the aircraft were bent backward.

The right door of the nose landing gear was opened outward wider than normal, and the scratch marks were found on the inner forward surface of the door. The scratch marks were found on the entire outer surface of the nose landing gear left door.

In addition, the scratch marks were found on the entire lower surface of the engine cowling in front of the nose landing gear well.

The rod end bearing at the tip of the actuator (nose landing

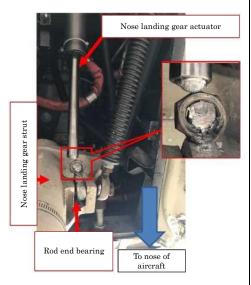


Photo 3 Damage on Nose landing gear

gear actuator) to move the nose landing gear up and down was fractured. The landing gear was in its down position even though the piston rod was bent. The engine mount frame at around the nose landing gear actuator mounting section was cracked.

(5) Broken rod end bearing

The rod end bearing was bent and fractured at an angle of about 90-degree on its lock nut section. In addition, the sliding section did not move smoothly.

The Report of the National Research and Development Agency, National Institute for Materials Science, which requested the surface of the broken section, states that the breaking of the rod end bearing is not attributable to the metal fatigue, but to the ductile fracture caused by the

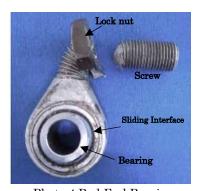


Photo 4 Rod End Bearing (Photo taken by National Institute for Materials Science)

bending load (Destruction with deformation due to excessive loading load). The process of the rod end bearing rupture is described as follows: The rod end bearing was buckled due to the compression load followed by the breaking of the bearing due to the excessive bending load. In addition, regarding that the movement on sliding section has not been smooth, the report states that it is not deniable that rust has developed in sliding interface.

(6) Landing gear

The landing gears of the aircraft are retractable and composed of the main landing gears under the left and right main wings and the nose landing gear under the nose section of the fuselage, the nose landing gear extends from backward to forward when extending it.

Operating each landing gear and keeping its position respectively controlled by individual actuator. The landing gear control lever actuates the electrical hydraulic pump, and the piston rod of the actuator on every landing gear extends or retracts. In the case of landing gear extension, when the piston rod fully extends, the switch piston inside each actuator is activated and the piston rod is held.

At the same time, when the switch interlocking with the switch piston would be activated,

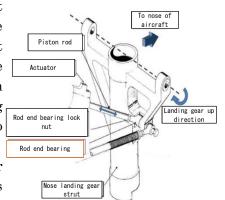


Figure 2: Nose Landing Gear Structure

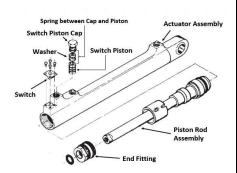


Figure 3: Actuator Structure

the supply of hydraulic pressure by the hydraulic pump has been stopped, and the three green lights on the instrument panel corresponding to each landing gear illuminate. A landing gear held in its down position is configured such that its extended position is not released unless the hydraulic pressure for retracting is supplied to the actuator and the switch piston is returned.

The position of each landing gear in its up and down position is set by adjusting the length of the rod end bearing on the actuator. (See Photo 5.)

(7) Maintenance on Rod End Bearing

Two nuts (Lock nut and Jam nut) are utilized when attaching a rod end bearing on a piston rod. In the Maintenance Manual of the same type of the aircraft, when the nose landing gear cannot be accommodated with the proper retracted position, it is allowable to use one nut (remove the jam

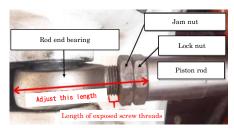


Photo 5 Length of Rod End Bearing (Other aircraft)

nut) but the maximum length of the exposed threads shall be 0.28 in (approximately seven mm).

Only the lock nut was utilized and it is highly probable that the exposed length was close to the maximum allowable exposure length based on the numbers of threads of the exposed part.

It is described in the Maintenance Manual of the same type of the
aircraft that such maintenance as lubrication shall be carried out on
the rod end bearing during the 100-hour inspection. It was confirmed
by the Maintenance Records that the 100-hour inspection had been
carried out.
Moreover, it could not be confirmed by the record that the rod end
bearing on the nose landing gear was replaced.

3. ANALYSIS

3.1 Involvement of	No
Weather	
3.2 Involvement of	No
Pilots	
3.3 Involvement of	Yes
Aircraft	
3.4 Analysis of	(1) The aircraft had a valid airworthiness certificate and had been
Findings	performed inspection and maintenance.
	(2) The ground speed of the aircraft when its propeller blades hit
	the runway surface is estimated to be about 45 kt. It is highly
	probable that the aircraft was reducing its speed despite the Pilot
	did not apply the brake on the aircraft.
	(3) It is highly probable that the aircraft became unable to move
	on the runway during the landing roll because the rod end bearing
	of the nose landing gear actuator was ruptured and consequently
	the nose landing gear was retracted.
	It is somewhat likely that the following sequence of events
	had occurred in the process until the rod end bearing had been
	ruptured:
	① The nose landing gear strut had leant to backward from the
	normal gear down position.
	② In addition to the impact load applied when the nose
	landing gear contacts the ground and the rearward load applied
	until the front wheel rotates (spin up) to the same
	circumferential speed as the forward speed, as the speed of the
	aircraft reduced during the landing roll, the load (the weight of
	the aircraft) applied on the nose landing gear increased and the
	compression load was applied to the actuator supporting the
	nose landing gear along its longitudinal direction.
	3 Buckling and excessive bending load occurred on the rod
	end bearing.
	4 After the thread on the rod end bearing was bent at an angle
	of about 90 degree, its connection section with the piston rod end
	was ruptured.
	⑤ Since the support by the nose landing gear actuator ceased,
	it was pulled in and the aircraft became unable to move on the

runway.

Regarding that the nose landing gear was leant backward from the normal position of its extended position, it is somewhat likely that the rod end bearing was bent because the adjustment of its fully extended position had been improper or the movement of the sliding area of the rod end bearing was restricted while the piston rod was fully extended.

4. PROBABLE CAUSES

In this serious incident, it is highly probable that the aircraft became unable to move on the runway during the landing roll because the rod end bearing of the nose landing gear actuator was ruptured and consequently the nose landing gear was retracted.

Regarding that the rod end bearing ruptured, it is somewhat likely that the compression load was applied to the actuator along its longitudinal direction because the nose landing gear strut leant backward from its normal fully extended position.